Is C3Po justified? *Modulation: how fast*?

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Modulation speed, P. Judge, HAO – p.1/13

A 500Hz (2k - 4k samples) polarization modulation
requirement was in an early Science Requirements
Document, but in the current version this derived
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- \checkmark hence, a rotating retarder is desirable.
- ✓ How fast do we need to rotate/modulate to adequately remove seeing-induced image distortions?



Possible modulation schemes (Elmore)

For a rotating retarder,

/ Slow retarder (16 samples/rotation up to 100 frames/sec).
 Single or dual beam analyzer. Dual beam analysis should consider, 10%, 1%, and 0.1% flat fielding and pixel registration from perfect to 1/2 pixel out.



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- Fast retarder (16 samples/rotation 1600 or greater shifts/sec with or without chopping analyzer. Four state FeLC/PEM)
 Single beam polarization analyzer.
- Slow retarder with a rapidly chopping analyzer. Single or
 Dual beam analysis with the same range of dual beam qualities.



Formalism

For seeing-induced image motion only, use Lites (1987):

 \checkmark R_i is pure solar Stokes vector. Measured signal in Stokes S_i is

$$S_{i}(x,y;t) \approx R_{i}(x,y;t) + \vec{\nabla}R_{i}(x,y;t) \cdot \vec{s}(t),$$

$$S_{i} \approx R_{i} \left(1 + \frac{|\nabla R_{i}|}{|R_{i}|} \sigma N(t)\right) \qquad (1)$$

$$= R_{i} \left(1 + \beta_{i} N(t)\right), \qquad (2)$$

 $\vec{s}(t) = \begin{pmatrix} x'-x \\ y'-y \end{pmatrix}$ is the seeing-induced image displacement at time t, N(t) is the image motion at time t (with unit rms), the seeing has rms σ , and the normalized power spectrum $P_N(\nu)$ is such that $\int_0^\infty P_N(\nu) d\nu = 1$.



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/ Lites showed

$$\sigma_{ri}^2 = (R_i \beta_i)^2 \int_0^\infty |\tilde{H}'_{ri}(\nu)|^2 P_N(\nu) \, d\nu.$$

where $\tilde{H}'_{ri}(\nu)$ is the Fourier transform of the product of the modulation function for input purely of parameter *i* with the demodulation function for parameter *r*.



Raw and tip-tilt corrected $P_N(\nu)$



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$\int_0^\infty |\tilde{H}'_{ri}(\nu)|^2 P_N(\nu) \ d\nu: \text{ASP scheme}$



Demodulation frequency = 16x retarder frequency!



$\int_0^\infty |\tilde{H}'_{ri}(\nu)|^2 P_N(\nu) \, d\nu: \text{ chopped 4}$ state ASP scheme



Demodulation frequency = 16x retarder frequency!



Stokes I $R_i\beta_i$ Magnetoconvection: Nordlund, Stein; Stokes: Keller











0.0 0.2 0.4 0.6 0.8 1.0 1.2 I



Stokes V $R_i\beta_i$ Magnetoconvection: Nordlund, Stein; Stokes: Keller



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Parameters for magnetoconvection

- \checkmark small flux concentration in intergranular lane
- $\checkmark\,$ Stokes R convolved with ATST psf 6302Å
- $\checkmark \mathbf{R} = (0.7, -0.00038, 0.0029, 0.043)^T$
- $\checkmark \frac{|\nabla \mathbf{R}|}{|\mathbf{R}|} = (8, 980, 66, 60)^T \operatorname{arcsec}^{-1}$
- ✓ AO corrected Rimmele power spectrum, $\sqrt{2}\sigma = 0.127$ arcsec
- ✓ 10 second integration time (from convective dynamics)





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/ fast dual beam = $10 \times \text{s/n}$ of slow dual beam





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 ✓ chopping affects only fast (makes V better, QU worse)





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